A novel modulation strategy for integrating digital sub-channels within a PAL/PAL plus signal

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A NOVEL MODULATION STRATEGY FOR INTEGRATING DIGITAL SUB-CHANNELS WITHIN A PAL/PAL PLUS SIGNAL

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Abstract—This paper presents an original methodology which facilitates the modulation of digital signals within the active video portion of a conventional analogue PAL/PALplus television signal. The resultant crosstalk distortion errors which ensue are analysed and a model postulated that enables optimization of a number of important system parameters. It will also be shown that applying this model enables a balancing of subjective quality with data-rate.

I. INTRODUCTION

Substantial research has been undertaken over the last few decades with the explicit goal of enabling digital data transmissions to be embodied within a standard analogue television (TV) channel. The potential benefits accruing from such an intent are manifold, since for a given infrastructure extra multimedia services are feasible. Supplementary programme information, electronic TV guides, multi-lingual high quality audio and special Personal Computer (PC) downloading services are only a flavour of some of the possibilities afforded.

Previous research activities which have explored the use of sub-channels within a television signal, have primarily focused upon high definition (HDTV) and extended definition (EDTV) compatibility approaches [1,2], where the extra resolution is analogue modulated, so that it can be transmitted within these channels. The crucial compatibility issue when attempting to integrate digital data within a TV signal, is to ensure that the appearance of any picture distortions is not perceptible, which in reality tends to involve a trade-off between subjective quality and achievable data rate. To accomplish this objective three distinct possibilities can be identified:

1) data insertion in the blanking period,
2) data insertion in the active video,
3) data insertion outside the video signal, but within the same channel.

In Europe, a practical example of TV data transmission from the first category, is the well-known Teletext system, which modulates digital information on the unused lines in the vertical blanking period. The maximum data rate that can be achieved however is far too low for multimedia applications. Another fully compatible system presented in [3], provides a raw 150kBit/s data rate using spread spectrum technology, while a proposition for the American NTSC television system, called VBI (Vertical Blanking Interval) [4], was made by WavePhore, USA. This system occupies the first ten lines of each field and thus also provides a 150kBit/s data rate.

Interestingly, another WavePhore system, called TVT1 includes data outside the video signal [4], by placing an additional carrier between the colour and sound carriers. This is an example of the third category, which also includes such systems as that proposed by Dinsel [5], involving an additional carrier, modulated by a 16 Quadrature Amplitude Modulation (QAM), which is subsequently modulated by the sound carrier. This technique enables a typical throughput of between 128 and 196kBit/s.

Summarising these general findings suggests that the maximum achievable data rate is bound to approximately 200 kB/s. To achieve higher rates means that the second of the above alternatives must be considered, where data is inserted within the active video signal. In adopting this strategy, one must always be mindful that such methods inevitably encroach upon the sensitive issue of compatibility. Early research in this area [6, 7] used a correlation decoder for demodulating the data signal, which was modulated with a subjective optimised carrier at very low amplitudes. Another novel approach was proposed by Ruppel [8], who employed QAM of the picture carrier and obtained a data rate of 500kBit/s.

The technique discussed in this paper also belongs to this second category and is based upon a QAM of the colour sub-carrier [9]. In [10, 11, 12] during the development of the European PALplus widescreen standard, a variant of this arrangement was proposed for modulating additional widescreen information. In practice however, the proposed method was purely analogue-based and never implemented as part of the standard.
II. OVERVIEW

A. Principles

In contrast to the NTSC-system, where the two colour difference signals I and Q are quadrature modulated, PAL alternates the phase of the V-component carrier between 90 and 270 degrees from line to line, where the U-component is fixed to the 0 degree carrier phase. Figure 1 shows the location for the two modulated colour components in the horizontal / vertical frequency plot of the PAL television signal. The switching leads to a spectral offset of the two colour components in the three dimensional frequency domain, with the V-carrier modulated on its 90-degree phase and the U-carrier on its 0-degree. Hence, both frequencies can be additionally modulated by using the respective orthogonal components and provide two sub-channels which are suitable for further digital transmission. For realisation, the carrier phase of the “digital U-component”, Du, must turn between 0 and 180 degrees from line to line during the carrier phase of Dv is fixed to 90 degrees. Figure 2a) displays this more graphically for the given colour and data vector F and D in two consecutive lines n and n+1. Their addition forms the output vector S, which undergoes the usual further processing before transmission. In the receiver, at the PAL line delay, the vector sum of two neighboured lines is derived so that the U and Dv signals are obtained from the in-phase and quadrature components respectively and also in the same way V and Du from the colour vector difference (Figure 2b)). This perfect possibility of separation is only valid if the neighboured lines have identical content, which is not what happens in reality so that cross talk distortions will occur.

The block diagram in Figure 3 provides an insight into the conceptual implementation of the aforementioned technique. The colour signals, U and V, are processed as usual with the subtle difference that a vertical lowpass, Hv(fy) and Hu(fy) component is added in each signal path (see next section). The data stream is initially split into two channels which operate at half the original data rate before subsequently form filtering. This filter together with the ensuing up-sampling and vertical interpolation is part of the two dimensional form filtering technique detailed in Section III. Following modulation as alluded to above, the resulting data vector is added to the colour and multiplexed with the luminance. At the decoder, after luminance / chrominance separation, the colour data signal is processed by the PAL line delay, which splits it into components whose carrier phase respectively alternates and remains fixed (V, Du and U, Dv respectively). Finally the demodulation provides the reconstruction of each signal. The post filters are necessary to suppress higher order frequency parts from the demodulation and for the data signal parts, to suppress the single sideband components from the colour signal. At the end, the two data channels are combined to rebuild the original data stream.
Another source of cross distortion is the converse scenario of the above discussion, where the colour is crossing over and affects the data channels. These errors are not so critical, because the issue of compatibility is not influenced and the subsequent disturbances impinge only upon the digital data stream, which is inherently more robust. Two different sources for these distortions can be distinguished. Firstly, the colour signals cross over and secondly inter-carrier crosstalk between the two data channels.

The inter-carrier crosstalk between data channels is limited due to the aforementioned spectral forming. In formalising the development of the proposed solution, the encoder-decoder implementation for the data stream is directly equivalent to the transmultiplexer structure proposed by Vetterli [15]. By selecting a special set of filter responses, all aliasing, amplitude and phase errors can be eliminated and perfect separation achieved. This however excludes the possibility of using the PAL line delay for data channel separation, so an additional filter set must be included in the configuration.

III. ENCODER DESIGN AND SUBJECTIVE PERFORMANCE

The encoder design discussed in this paper concentrates primarily on a number of different possible spectral forming filters for the data signals, to avoid inter-carrier cross-colour noise distortion. Their role is most crucial in the context of compatibility and subjective performance.
A. Theoretical analysis

An understanding of the three dimensional spectral position is provided in Figure 4. The locations of the modulated colour signals U and V, are given with their carrier position at the centre. The spectra of the embedded data signals are in theory uniformly distributed along the three axes of the 3-D frequency plot, since each data value is uncorrelated both with respect to adjacent line and frame samples. To constrain these spectra to specific locations so avoiding the aforementioned crosstalk effects, form filtering must be applied. Horizontal forming is performed using the traditional filter included to avoid intersymbol interference and ensures that the bandwidth is limited to 0.5 MHz. In addition, either vertical or temporal filtering is necessary to provide non-overlapping frequency regions for the data spectra. Due to the fact that for the colour signal separation at the decoder a vertical filter, the PAL line delay, is used, also for the data channel vertical forming filters are essential.

The vertical filters providing these spectral locations for each data component have to be lowpass. Analysing the distortions raising from crossing over into the colour channels, the data signals passing through mentioned vertical lowpass before subsequently processed by the PAL line delay, which is a sine-shaped high pass response for Dv. Similar argument can be applied to Du, so the crosstalk attenuation response is the same in both cases and can be readily computed from the relationship:

\[ C_A(f_y) = H_2(f_y) \cdot H_0(f_y) \]  \hspace{1cm} (1)

where \( H_2(f_y) \) is the sine-shaped PAL line delay separation, and \( H_0(f_y) \) the vertical low pass forming filter for the data signal at the encoder.

Quantifying the aforementioned cross-distortions is very difficult since they only interfere in the colour channel. Their appearance is blocky colour noise which is unusual in comparison with normal noise degradation's and therefore is perceptually very annoying. To provide a quantitative measure, the noise power accruing from the crosstalk data signals is evaluated so both the signal to noise ratio within each colour channel (SNR) together with the display signal to noise ratio (DSNR) can be derived. This latter measure is similar to the model published in [16].

Assuming the data signal \( U_0 \) has a uniform probability distribution function with zero mean over a range from \( -\alpha \) to \( \alpha \), the noise power can be computed directly from the variance \( \sigma^2 \). Depending on the number of symbol levels per data channel, which will be for example N=2 for 4 QAM, N=4 for 16 QAM \(^1\) and so on, the following relationship can be used:

\[ \sigma^2 = \frac{\alpha^2 \cdot N + 1}{3 \cdot N - 1}; \quad N \geq 2 \]  \hspace{1cm} (2)

Assuming the conditions of a noise-free transmission, which means ideal filter characteristics for both luminance and chrominance splitting, as well as chroma demodulation at the receiver, so that only the colour difference signals are effected by cross colour noise distortions. The noise power in each colour channel introduced from the data signal is then given as:

\[ P_n = \int \int \sigma^2 |H_x(f_x)|^2 \cdot |C_x(f_x)|^2 \cdot df_x \cdot df_y \]  \hspace{1cm} (3)

where \( C_A(f_y) \) is the crosstalk attenuation response introduced in Eq. 1 and \( H_x(f_x) \) the horizontal forming filter. \( f_x \) and \( f_y \) are the horizontal and vertical sampling frequency, respectively. If no vertical forming filter is used in the encoder, so that \( C_A(f_y) = H_0(f_y) \), Eq. 3 is simplified to

\[ P_n = \frac{\sigma^4 \cdot f_x}{2} \int_{0}^{f_x} |H_x(f_x)|^2 \cdot df_x \]  \hspace{1cm} (4)

In evaluating the noise performance, the eye weighting function has to be taken into account. In this case however, the noise bandwidth is less than 0.5 MHz where the eye's perception has nearly no degradation [17]. The same situation is assumed for the luminance/chrominance separation and also for the

\(^1\) The noise power is evaluated separately for each channel.
colour post filters, so that only $C_A(t_n)$ and $H(t_n)$ have to be considered.

From Eq. 3 the signal to noise ratio (SNR) is given as

$$\text{SNR}_{[dB]}(u,v) = 10 \log \frac{P_{u,v}}{P_n}$$

The maximum peak-to-peak signals for U and V are different and are [18]:

- $U = 0.612 V_{pe}$
- $V = 0.861 V_{pe}$

So the inter carrier crosstalk can be qualified:

$$\text{SNR}_{u} = 10 \log \frac{0.342 R_{u}^{2} + 0.566 G_{u}^{2} + 0.22 B_{u}^{2}}{P_n}$$

$$\text{SNR}_{v} = 10 \log \frac{0.59 G_{v}^{2} + 0.11 B_{v}^{2}}{P_n}$$

From this objective SNR measure, a more subjectively oriented method is derived, whose basis is a modification of the DSNR definition in [16]. This technique takes cognisance of the fact that the crosstalk noise encroaches upon the principle of constant luminance, which implies an additional crosstalk into the luminance component, because of the non-linearity of the picture tube, a phenomena known as the gamma law.

Eq. 3 quantifies the distortion within each colour signal, $U'$ and $V'$. To assess the visibility at the display, the expression for signal plus noise at the output of the decoder matrix must be derived. With $R' - Y' = 1.14V'$ and $B' - Y' = 2.03U'$ the three distorted primary colour signals are given as:

$$R' + n_R = R + 1.14 \sqrt{P_n}$$

$$G' + n_G = G + 0.96 \sqrt{P_n}$$

$$B' + n_B = B + 2.03 \sqrt{P_n}$$

where $R' = R_{1r}$, $G' = G_{1r}$, $B' = B_{1r}$ are the pre-gamma corrected colour signals and $n_R$, $n_G$, $n_B$ the respective cross colour noise distortions. The displayed luminance $Y_D$ at the output of the display tube can be obtained by separately weighting the three primary colour signals and adding each term after applying the gamma law [16].

$$Y_D = 0.3(R + 1.14 \sqrt{P_n})^{\gamma_H} + 0.59(G + 0.96 \sqrt{P_n})^{\gamma_H} + 0.11(B + 2.03 \sqrt{P_n})^{\gamma_H}$$

Using the relationship $(1+a)^{\gamma_H} = 1 + \gamma_H a$, for $a << 1$ Eq. 8 can be written as

$$Y_D = 0.3 + 0.59G + 0.11B$$

and letting $\delta = 1 - \frac{1}{\gamma_H}$ and adding signal terms in voltage and noise terms in power [16]

$$Y_D = 0.3R + 0.59G + 0.11B + \gamma \sqrt{P_n} \sqrt{(0.342 R^2)^2 + (0.566 G^2)^2 + (0.22 B^2)^2}$$

The DSNR is then given by

$$\text{DSNR} = 20 \log \frac{\gamma \sqrt{P_n} \sqrt{(0.342 R^2)^2 + (0.566 G^2)^2 + (0.22 B^2)^2}}{P_n}$$

which can be computed for a given $P_n$ and $\gamma$, where $P_n$ is direct related to both $\alpha$, the data signal amplitude and the number of symbol levels $N$. For increasing $N$, Eq. 1 shows that $\sigma^2$ moves to a threshold of $1/3$ for $\alpha = 1$, so a 16-QAM or 64-QAM, $N=4$ or $N=8$ respectively, will balance the DSNR gain with complexity.

B. Filter Optimisation

Two methods will be discussed for the implementation of the vertical spectral forming filter, namely vertical partial response coding and a vertical interpolation technique.

Partial response coding performs a spectral forming by introducing more than two symbols and therefore an energy concentration within a smaller bandwidth. If Duobinary coding is considered for instance, the data spectrum becomes cosine shaped, which reduces the crosstalk effects, the cross talk attenuation of $C_A(t_n)$ is however insufficient. Higher order partial response codes will increase this attenuation and the overall subjective performance, but also the number of symbol levels, which decreases the transmission robustness.

The other spectral forming technique involves transmitting data only every $n$th line, where $n$ is the interpolation factor. This has the effect of reducing the bandwidth of the data signal by $1/n$. An interpolation filter interpolates the omitted lines and performs the vertical spectral forming. To preserve the data rate a higher order QAM technique is suggested which gives $1/n$, $2/n$ or $3/n$ for a $4-, 16-$ or $64-$QAM respectively of the original data rate. At the decoder, to ensure optimal reconstruction of the data signals, the overall vertical filter chain during transmission must maintain the original data samples. This prerequisite is fulfilled provided every $n^{th}$ sample of the overall filter’s impulse
response is zero in the aforementioned cases. A specially designed interpolation filter family has therefore to be applied at the encoder, exhibiting these properties, and then exclude the other vertical filters of the chain, which is the PAL line delay; if this will used for separation of the data channels. Otherwise the PAL line delay must be considered only for the compatibility issue and for the decoding process additional filters must be applied.

The frequency response of any filter where only the \( n^{th} \) coefficient is non-zero has the property of providing an attenuation of more than 6dB at \( 1/n \) of the Nyquist frequency. Excluding the frequency response of the PAL line delay which is cosine shaped, such attenuation is limited and nearly independent from the filter design. This confines any crosstalk improvement within the filter design process, so that only minor changes are possible by varying, for example, filter complexity.

A combination of the interpolation technique together with the duobinary coding will provide a possible solution of this lemma. A duobinary coded signal spectrum is cosine shaped, so it has a zero at the Nyquist frequency. Up-sampling by a factor of \( n \) moves this null point to \( 1/n \) of the new Nyquist frequency and thus introduces a notch at the aforementioned critical location. The pyrrhic effect however, is that this is only possible with two symbol levels per data channel leading to a lower data rate, otherwise, due to the combination, to much symbol levels occur.

IV. DISCUSSION OF RESULTS

The technique presented in this paper is based upon modulating the active video part of a PAL signal. To be compatible with the PALplus standard, only 432 of the total 576 active PAL lines are available, which forms the kernel 16:9 widescreen signal. The remaining 144 lines are reserved for the transmission of the so-called vertical helper signal. The ensuing discussion and results relate to the 432 line core signal. The helper components remain unaffected, also for a pure PAL signal.

For the initial simulations the horizontal form filter, avoiding inter-symbol interference, is chosen with a roll off slope of 0.5. The overall data channel bandwidth is, as given in II.B.:

\[
f_{\text{data}} = 5 \text{MHz} \cdot 4.433 \text{ MHz} = 0.567 \text{ MHz}
\]

so that the bit duration might not exceed

\[
T_{\text{bit}} = \frac{1}{2f_{\text{data}}} = 1.323 \mu s
\]

With an active line length of 52\( \mu s \), this results in a maximum of 39 symbols per line and per additional data channel. For simplification of the simulation and to avoid the worst case, 36 symbols are used, so for both channels 72 symbols per line are available and every line contains an integer number of bytes. The overall data rate provided can be derived as follows:

\[
r = \frac{72 \text{ symbols}}{\text{line}} \cdot \frac{432 \text{ line}}{\text{frame}} \cdot \frac{25 \text{ frame}}{s} \cdot \frac{\text{ldN} \text{ Bits}}{\text{symb}} \cdot \frac{1}{n} = \frac{777.6 \text{ KBits}}{s}
\]

where \( N \) is the number of symbol levels per channel and \( n \) the interpolation factor (Figure 5).

The roll-off filter design is straight forward and implemented as usual separated in a pre- and post filter at the encoder and decoder, respectively. Considering the vertical forming filter, not much flexibility in designing this filter is given, neither for the partial response coding, where the vertical filter are fixed due to the chosen order, nor for the interpolation technique as alluded in the previous section. The most important parameters, which having an impact to the overall efficiency, that is data rate and subjective quality, are the amplitude of the data signal, \( \alpha \), the number of symbol levels, \( N \), and the interpolation factor \( n \). With Eq. 1 and Eq. 2 the power of the intercarrier crosstalk can be derived within each colour channel and an objective quality is given using Eq. 10.
Table 1: Comparison of different crosstalk noise

<table>
<thead>
<tr>
<th>Example</th>
<th>N</th>
<th>n</th>
<th>r</th>
<th>Pn</th>
<th>α=0.15</th>
<th>SNRl0</th>
<th>SNRl1</th>
<th>Pn</th>
<th>α=0.075</th>
<th>SNRl0</th>
<th>SNRl1</th>
</tr>
</thead>
<tbody>
<tr>
<td>P1</td>
<td>2</td>
<td>1</td>
<td>777.6</td>
<td>3.574 \times 10^4</td>
<td>30.21 dB</td>
<td>33.17 dB</td>
<td>0.934 \times 10^4</td>
<td>33.17 dB</td>
<td>39.19 dB</td>
<td></td>
<td></td>
</tr>
<tr>
<td>P2</td>
<td>2</td>
<td>1</td>
<td>777.6</td>
<td>1.768 \times 10^4</td>
<td>30.21 dB</td>
<td>33.17 dB</td>
<td>0.934 \times 10^4</td>
<td>33.17 dB</td>
<td>39.19 dB</td>
<td></td>
<td></td>
</tr>
<tr>
<td>I1</td>
<td>2</td>
<td>2</td>
<td>388.8</td>
<td>3.015 \times 10^4</td>
<td>33.91 dB</td>
<td>33.91 dB</td>
<td>0.753 \times 10^4</td>
<td>39.93 dB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>I2</td>
<td>2</td>
<td>2</td>
<td>777.6</td>
<td>1.675 \times 10^4</td>
<td>33.91 dB</td>
<td>33.91 dB</td>
<td>0.753 \times 10^4</td>
<td>39.93 dB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>I3</td>
<td>2</td>
<td>3</td>
<td>259.2</td>
<td>0.705 \times 10^4</td>
<td>37.76 dB</td>
<td>40.22 dB</td>
<td>0.176 \times 10^4</td>
<td>43.28 dB</td>
<td>46.24 dB</td>
<td></td>
<td></td>
</tr>
<tr>
<td>I4</td>
<td>2</td>
<td>3</td>
<td>518.4</td>
<td>0.392 \times 10^4</td>
<td>39.82 dB</td>
<td>42.77 dB</td>
<td>0.098 \times 10^4</td>
<td>45.83 dB</td>
<td>48.79 dB</td>
<td></td>
<td></td>
</tr>
<tr>
<td>P1/I1</td>
<td>2</td>
<td>2</td>
<td>388.8</td>
<td>0.628 \times 10^4</td>
<td>37.76 dB</td>
<td>40.22 dB</td>
<td>0.157 \times 10^4</td>
<td>43.78 dB</td>
<td>46.73 dB</td>
<td></td>
<td></td>
</tr>
<tr>
<td>P1/I4</td>
<td>2</td>
<td>3</td>
<td>259.2</td>
<td>0.160 \times 10^4</td>
<td>43.69 dB</td>
<td>46.65 dB</td>
<td>0.040 \times 10^4</td>
<td>49.71 dB</td>
<td>52.67 dB</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Three different design methods together with their parameters are compared in Table 1. Px refers to partial response coding, Ix to interpolation and PxIx to the combination of both methods. I1 and I4 are designed as alluded in Sec. IIIB, with an amplification of the interpolation factor, n, to keep the data signal power independent from the interpolation factor. The corresponding filter responses \( H_d(f) \) and \( C_a(f) \) are given from with Figure 7. It is obvious that with an increasing cross talk attenuation the achieving data rate decreases. Giving the priority to the subjective picture quality the values from example I4, P1/I1 and P1/I4 produce the best compromise, where the 16 QAM version of I4 provides a superb bit rate efficiency. The data amplitude, \( \alpha \), should be within the limits of 0.075 and 0.15 in relation to the normalised video range. A value of 0.15 causes an overshoot of 20% of the resulting video signal (Figure 6), which is a little bit less than for saturated yellow and therefore acceptable. Further \( \alpha \) should not be below 0.075, because of an increasing data error rate in noisy transmission channels.

Table 2 shows the DSNR of an EBU colour bar for the examples given in Table 1. It gives a very good impression of what distortions are definite visible within the possible signal parts of a video signal. Surely, the degradation’s are more visible in dark uniform areas than in bright parts. The DSNR varies within a range of approximately 20 dB depending on the form filtering. For values greater than 35dB, almost no visible distortions are perceived by non expert viewers.

The previous discussion relates only to the issue of compatibility, which as alluded earlier is of paramount importance and parameter settings are consequently chosen to reflect this. Also of interest however are the properties of the data channels, is respect of their achievable data rate and also the Bit Error Rate (BER). The data rates have already been discussed, the BER is directly dependent upon the data signal amplitude \( \alpha \), and the numbers of signal levels, N. Figure 9 and Figure 10 show the measured eye patterns and corresponding signal space for 2 and 4 signal levels per data channel, respectively. The asymmetry shape of the symbol positions is caused by arithmetic rounding being used in the signal processing. Despite this, the example reveals that perfect data reconstitution is certainly possible. This ideal situation inevitably deteriorates when white Gaussian noise is added during transmission. The noise degrades the symbol positions within the signal space, so they become less and less defined and the openness of the eye narrows, leading to a increased probability of bit errors with the number of symbol levels. Figure 8 compares the examples for signal to noise ratios within the range 30dB to 40 dB for the 16 QAM case. The 4 QAM together with the duo-binary coding technique provides a BER greater than \( 10^{-3} \) within these tests.

Another source of bit errors are introduced from high vertical colour frequencies, which cross over into the data channel. Due to the probability occurrence of those frequencies the resulting errors appear as burst errors. The previous mentioned vertical filter in the colour signal paths will prevent these effects.

Figure 6: EBU colour bar added with the modulated data signal
Table 2: DSNR of an EBU Colour bar for various examples

<table>
<thead>
<tr>
<th>Example</th>
<th>$\alpha=0.15$</th>
<th>$\alpha=0.75$</th>
<th>$\alpha=0.15$</th>
<th>$\alpha=0.75$</th>
<th>$\alpha=0.15$</th>
<th>$\alpha=0.75$</th>
<th>$\alpha=0.15$</th>
<th>$\alpha=0.75$</th>
</tr>
</thead>
<tbody>
<tr>
<td>P1</td>
<td>35.8686 dB</td>
<td>34.9095 dB</td>
<td>33.5502 dB</td>
<td>32.6968 dB</td>
<td>32.3453 dB</td>
<td>31.1742 dB</td>
<td>26.1624 dB</td>
<td>32.8450 dB</td>
</tr>
<tr>
<td>P2</td>
<td>33.8154 dB</td>
<td>32.1381 dB</td>
<td>30.7780 dB</td>
<td>29.9254 dB</td>
<td>29.5739 dB</td>
<td>28.4028 dB</td>
<td>23.3910 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>P2</td>
<td>39.7872 dB</td>
<td>38.1099 dB</td>
<td>36.7560 dB</td>
<td>35.8971 dB</td>
<td>35.5457 dB</td>
<td>34.3746 dB</td>
<td>29.3627 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>I1</td>
<td>37.5223 dB</td>
<td>35.8450 dB</td>
<td>34.4857 dB</td>
<td>33.6323 dB</td>
<td>33.2808 dB</td>
<td>32.1097 dB</td>
<td>27.0979 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>I1</td>
<td>34.0501 dB</td>
<td>32.3728 dB</td>
<td>31.0135 dB</td>
<td>30.1601 dB</td>
<td>29.8086 dB</td>
<td>28.6375 dB</td>
<td>23.6257 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>I1</td>
<td>40.0681 dB</td>
<td>38.3908 dB</td>
<td>37.0315 dB</td>
<td>36.1781 dB</td>
<td>35.8266 dB</td>
<td>34.6555 dB</td>
<td>29.6437 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>I4</td>
<td>37.8084 dB</td>
<td>36.1311 dB</td>
<td>34.7718 dB</td>
<td>33.9183 dB</td>
<td>33.5669 dB</td>
<td>32.3958 dB</td>
<td>27.3839 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>I4</td>
<td>43.8351 dB</td>
<td>42.1578 dB</td>
<td>40.7986 dB</td>
<td>39.9451 dB</td>
<td>39.5936 dB</td>
<td>38.4225 dB</td>
<td>33.4107 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>I4</td>
<td>40.3574 dB</td>
<td>38.6801 dB</td>
<td>37.3208 dB</td>
<td>36.4674 dB</td>
<td>36.1159 dB</td>
<td>34.9448 dB</td>
<td>29.9330 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>I4</td>
<td>46.3780 dB</td>
<td>44.7007 dB</td>
<td>43.3414 dB</td>
<td>42.4880 dB</td>
<td>42.1365 dB</td>
<td>40.9654 dB</td>
<td>35.9536 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>P1/I1</td>
<td>38.3106 dB</td>
<td>36.6334 dB</td>
<td>35.2741 dB</td>
<td>34.4206 dB</td>
<td>34.0692 dB</td>
<td>32.8980 dB</td>
<td>27.8862 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>P1/I1</td>
<td>44.3312 dB</td>
<td>42.6540 dB</td>
<td>41.2947 dB</td>
<td>40.4412 dB</td>
<td>40.0898 dB</td>
<td>38.9186 dB</td>
<td>33.9068 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>P1/I4</td>
<td>44.2490 dB</td>
<td>42.5717 dB</td>
<td>41.2125 dB</td>
<td>40.3590 dB</td>
<td>40.0076 dB</td>
<td>38.8364 dB</td>
<td>33.8246 dB</td>
<td>34.9095 dB</td>
</tr>
<tr>
<td>P1/I4</td>
<td>50.2696 dB</td>
<td>48.5923 dB</td>
<td>47.2331 dB</td>
<td>46.3796 dB</td>
<td>46.0282 dB</td>
<td>44.8570 dB</td>
<td>39.8452 dB</td>
<td>34.9095 dB</td>
</tr>
</tbody>
</table>

V. CONCLUSIONS

The paper introduces a novel modulation possibility which enables embedded digital subchannels within a standard video signal. The technique uses the active video part, so that crosstalk distortions occur. These degradation of compatibility has been fully analyzed and qualified. The concept of a more dimensional form filtering is proposed to suppress these effects, which, however, balance the data rate efficiency. Looking at noisy transmission channels, the proposed system provides acceptable bit error rates for signal to noise ratios better than 30 dB.

The subjective quality of the standard video signal, data rate and also the noise robustness are the major properties, which compromises each other. The best solution is found for the example P1/I1 with the priority on subjective quality. Shifting the focus a bit more to the data rate efficiency, the 16 QAM example of I4 is the best.

As mentioned earlier, only the center signal is used for additional modulation, which is ¾ of the overall picture space. To improve bit rate efficiency the consistency of the proposed modulation, or a modification of it, with the PALplus helper is currently under development.
Schmidt, Buchwald and Dooley: A Novel Modulation Strategy for Integrating Digital Sub-Channels within a PAL/PAL Plus Signal

Figure 8: Measured bit error rate (BER) for the 16 QAM approach

Figure 9: Eye pattern and signal space for 4 QAM

Figure 10: Eye pattern and signal space for 16 QAM

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VII. BIBLIOGRAPHIES

Gunnar Schmidt (M'93) was born in Braunschweig, Germany in 1966. He received his Dipl.-Ing. degree in Electronics and Communication Technology in 1990 from the Fachhochschule Braunschweig/Wolfenbuettel, Germany. From 1990 to 1997 he worked with the video
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